



上海交通大学  
SHANGHAI JIAO TONG UNIVERSITY



# Introduction to Marine Hydrodynamics

(NA235)

Department of Naval Architecture and Ocean Engineering

School of Naval Architecture, Ocean & Civil Engineering

Shanghai Jiao Tong University



# Review



**Pathline equation:**

$$\frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w} = dt$$

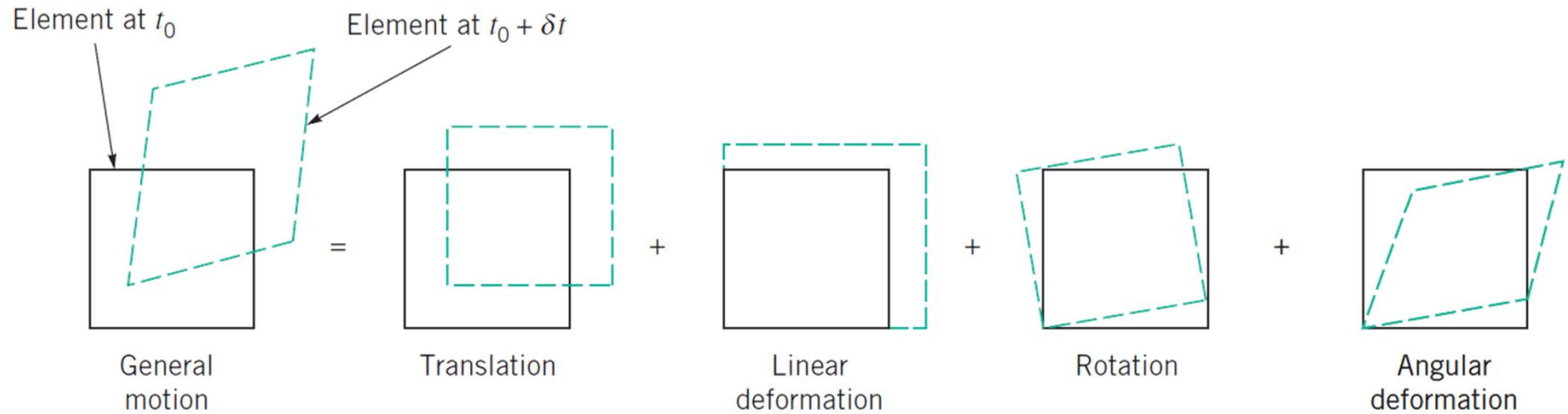


**Streamline equation:**

$$\frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w}$$



- Motion of fluid elements**



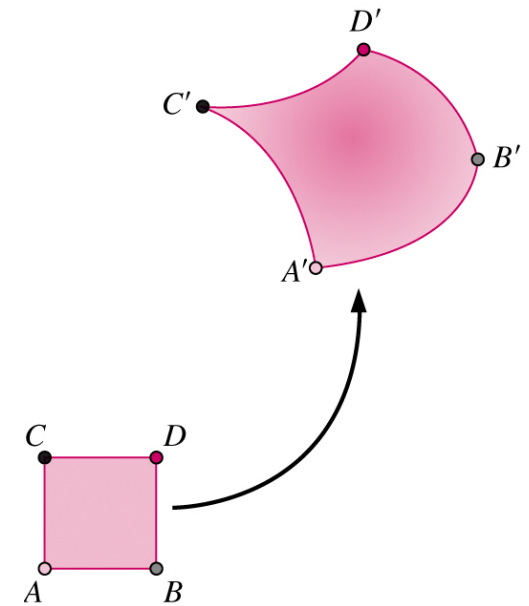


# Review

$$\mathbf{V}_{M'} = \left[ \underbrace{\underline{u}}_{(1)} + \underbrace{\omega_z dy + \omega_y dz}_{(2)} + \underbrace{\varepsilon_{xx} dx}_{(3)} + \underbrace{\varepsilon_{xy} dy + \varepsilon_{xz} dz}_{(4)} \right] \mathbf{i} + (\dots) \mathbf{j} + (\dots) \mathbf{k}$$

General motion = {

- Translation (1)
- +
- Rotation (2)
- +
- Dilatation (3) (change in volume)
- +
- Angular deformation (4) (change in shape)





# Review

## Shear strain rate – angular deformation

$$\epsilon_{xy} = \frac{1}{2} \left( \frac{d\alpha}{dt} + \frac{d\beta}{dt} \right) = \frac{1}{2} \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right)$$

$\epsilon_{xy} > 0$ , AOB decreases

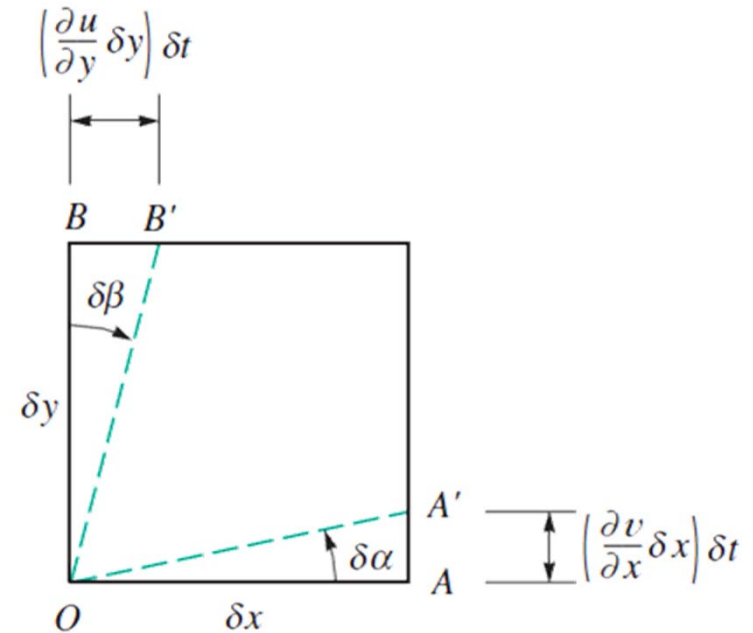
$$\epsilon_{yz} = \frac{1}{2} \left( \frac{\partial w}{\partial y} + \frac{\partial v}{\partial z} \right); \quad \epsilon_{zx} = \frac{1}{2} \left( \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right)$$

## Rate of rotation

$$\omega_z = \frac{1}{2} \left( \frac{d\alpha}{dt} - \frac{d\beta}{dt} \right) = \frac{1}{2} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$$

$\omega_z > 0$ , counterclockwise rotation

$$\omega_x = \frac{1}{2} \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right); \quad \omega_y = \frac{1}{2} \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right)$$



*Rotation with/w.o. deformation?*

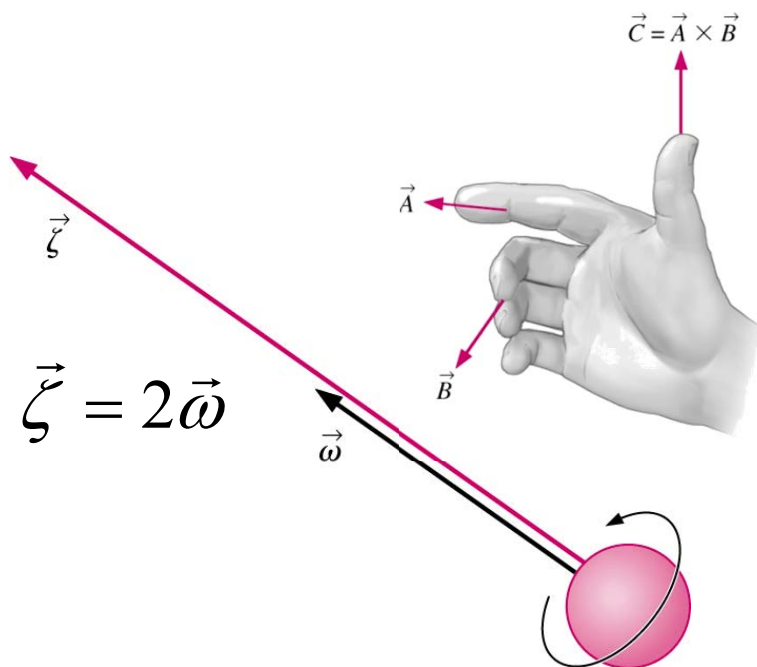


## 2.3 Deformation and Rotation of Fluid Elements

shear rate tensor  $\mathbf{E} = \varepsilon_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$

rate of rotation  $\boldsymbol{\omega} = \omega_x \vec{i} + \omega_y \vec{j} + \omega_z \vec{k} = \frac{1}{2} \boldsymbol{\zeta}$  (vorticity)

vorticity  $\boldsymbol{\zeta} = \boldsymbol{\Omega} = \nabla \times \mathbf{V}$  (curl of velocity)



$$= \begin{vmatrix} \vec{i} & \vec{j} & \vec{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ u & v & w \end{vmatrix}$$

$$= \underbrace{\left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right)}_{2\omega_x} \vec{i} + \underbrace{\left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right)}_{2\omega_y} \vec{j} + \underbrace{\left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)}_{2\omega_z} \vec{k}$$



## 2.3 Deformation and Rotation of Fluid Elements

Helmholtz decomposition can be written in tensor form:

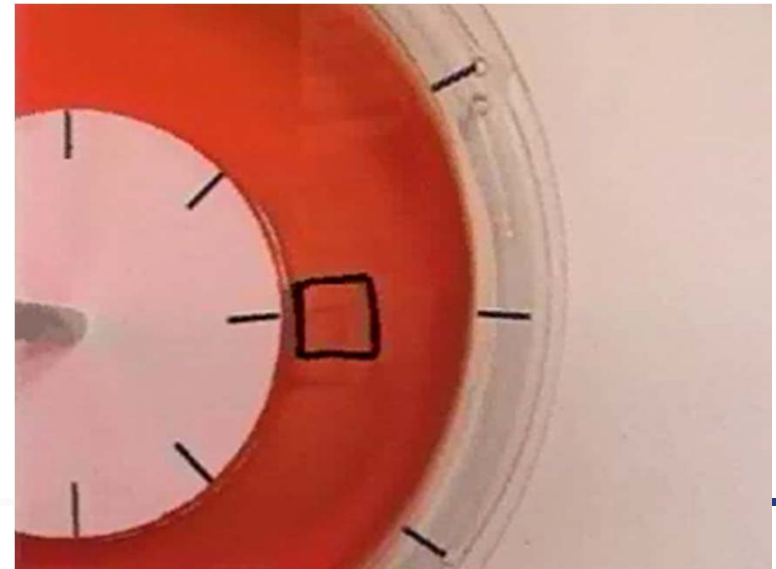
$$\text{Let } \delta \mathbf{r} = dx \mathbf{i} + dy \mathbf{j} + dz \mathbf{k}$$

$$\mathbf{V} = \mathbf{V}_0 + \mathbf{E} \cdot \delta \mathbf{r} + \boldsymbol{\omega} \times \delta \mathbf{r}$$

Rate of translation

Strain rate

Rate of rotation/angular velocity



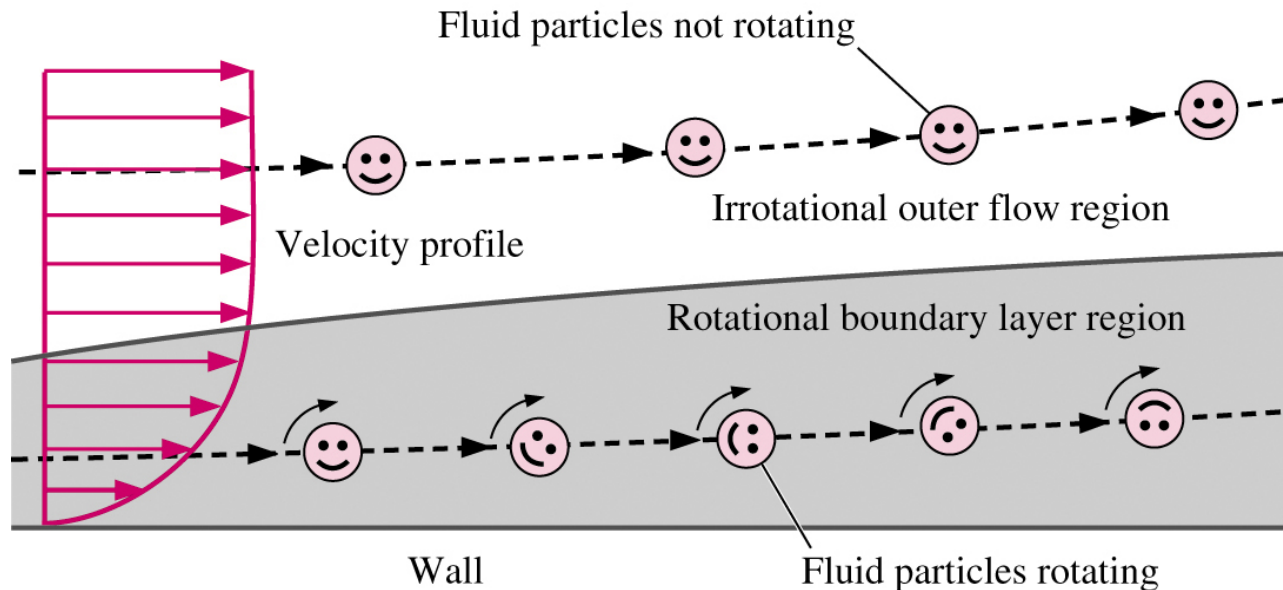


## 2.4 Rotational and Irrotational Flows

**Definition:** If the vorticity in a flow field is zero,  $\vec{\Omega}=0$ , the fluid particles are not rotating, the flow in that region is called **irrotational**. Otherwise, the flow in that region is called **rotational**.

$$\vec{\Omega} = (\Omega_x, \Omega_y, \Omega_z) = 0$$

$$\Omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0, \quad \Omega_x = \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} = 0, \quad \Omega_y = \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} = 0$$







## 2.4 Rotational and Irrotational Flows

### Application 1

The irrotational flow condition in the  $xy$ -plane in Cartesian coordinates is:  $\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0$

Derive the expression of irrotational flow condition in plane polar coordinates.

**Solution:** the relationship between Cartesian coordinates  $(x, y)$  and polar coordinates  $(r, \theta)$  is:

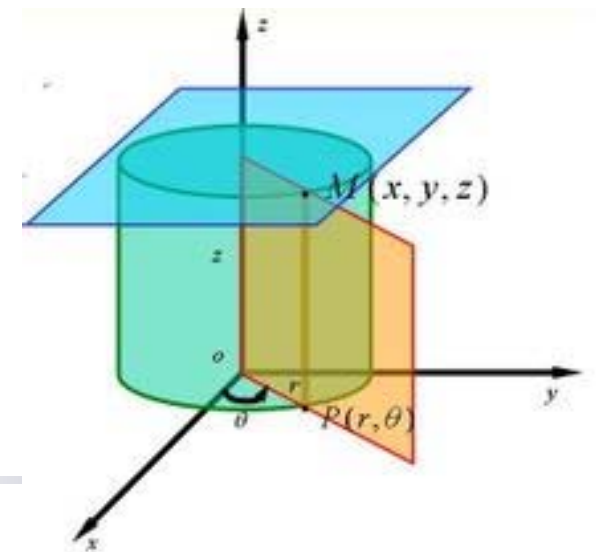
$$x = r \cos \theta, \quad y = r \sin \theta$$

where  $r = \sqrt{x^2 + y^2}$      $\theta = \arctan\left(\frac{y}{x}\right)$

The relationships between the velocities in the two coordinates system are:

$$u = v_r \cos \theta - v_\theta \sin \theta$$

$$v = v_r \sin \theta + v_\theta \cos \theta$$





## 2.4 Rotational and Irrotational Flows

The relationships between the differential operators are:

$$\frac{\partial}{\partial r} = \frac{\partial}{\partial x} \frac{\partial x}{\partial r} + \frac{\partial}{\partial y} \frac{\partial y}{\partial r} = \cos \theta \frac{\partial}{\partial x} + \sin \theta \frac{\partial}{\partial y}$$

$$\frac{\partial}{\partial \theta} = \frac{\partial}{\partial x} \frac{\partial x}{\partial \theta} + \frac{\partial}{\partial y} \frac{\partial y}{\partial \theta} = -r \sin \theta \frac{\partial}{\partial x} + r \cos \theta \frac{\partial}{\partial y}$$

Thus:

$$\frac{\partial}{\partial x} = \cos \theta \frac{\partial}{\partial r} - \sin \theta \frac{\partial}{r \partial \theta}$$

$$\frac{\partial}{\partial y} = \sin \theta \frac{\partial}{\partial r} + \cos \theta \frac{\partial}{r \partial \theta}$$



## 2.4 Rotational and Irrotational Flows

The **irrotational flow condition** in Cartesian coordinates is:

$$\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0$$

Transformed to polar coordinates:

$$\begin{aligned} \frac{\partial v}{\partial x} &= \left( \cos \theta \frac{\partial}{\partial r} - \sin \theta \frac{\partial}{r \partial \theta} \right) (v_r \sin \theta + v_\theta \cos \theta) \\ &= \sin \theta \cos \theta \frac{\partial v_r}{\partial r} + v_r \cos \theta \cdot 0 - \sin^2 \theta \frac{\partial v_r}{r \partial \theta} - \frac{v_r}{r} \sin \theta \cos \theta \\ &\quad + \cos^2 \theta \frac{\partial v_\theta}{\partial r} + v_\theta \cos \theta \cdot 0 - \sin \theta \cos \theta \frac{\partial v_\theta}{r \partial \theta} + \frac{v_\theta}{r} \sin^2 \theta \\ \frac{\partial u}{\partial y} &= \left( \sin \theta \frac{\partial}{\partial r} + \cos \theta \frac{\partial}{r \partial \theta} \right) (v_r \cos \theta - v_\theta \sin \theta) \\ &= \sin \theta \cos \theta \frac{\partial v_r}{\partial r} + v_r \sin \theta \cdot 0 + \cos^2 \theta \frac{\partial v_r}{r \partial \theta} - \frac{v_r}{r} \sin \theta \cos \theta \\ &\quad - \sin^2 \theta \frac{\partial v_\theta}{\partial r} - v_\theta \sin \theta \cdot 0 - \sin \theta \cos \theta \frac{\partial v_\theta}{r \partial \theta} - \frac{v_\theta}{r} \cos^2 \theta \end{aligned}$$



## 2.4 Rotational and Irrotational Flows



$$\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = (\cos^2 \theta - \sin^2 \theta) \frac{\partial v_\theta}{\partial r} + (\sin^2 \theta - \cos^2 \theta) \frac{v_\theta}{r} - (\sin^2 \theta + \cos^2 \theta) \frac{\partial v_r}{r \partial \theta} = 0$$

i.e.,

$$\frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} - \frac{\partial v_r}{r \partial \theta} = 0$$

Or,

$$\frac{\partial(rv_\theta)}{\partial r} - \frac{\partial v_r}{\partial \theta} = 0$$



## 2.4 Rotational and Irrotational Flows

### Application 2

For a two-dimensional flow field, the velocity is given as:

$$u = -\omega y, \quad v = \omega x$$

Is this flow rotational or irrotational? Will the fluid element deform or not?

**Solution:**

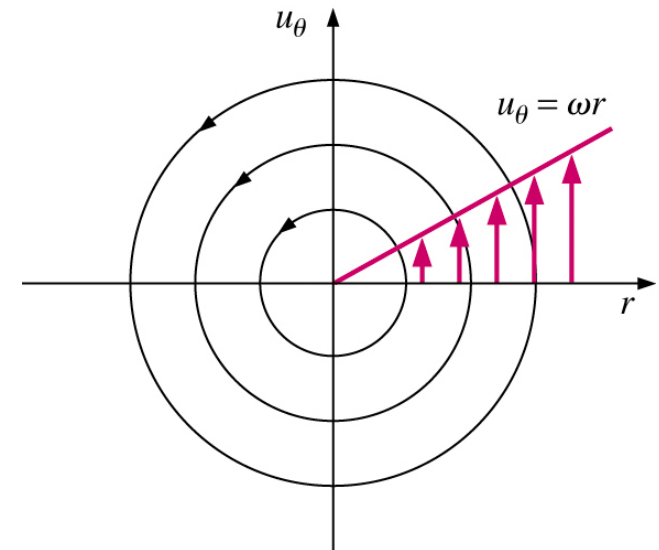
$$\Omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 2\omega, \quad \Omega_x = 0, \quad \Omega_y = 0$$

The flow is rotational

$$\varepsilon_{xx} = \varepsilon_{yy} = \varepsilon_{zz} = 0$$

$$\varepsilon_{xy} = \varepsilon_{xz} = \varepsilon_{yz} = 0$$

There is no deformation of the fluid element. This is used to describe the flow in the core region of a tornado.





## 2.4 Rotational and Irrotational Flows

### Application 3

A two-dimensional flow field the velocity is given as: ,

$$u = -\frac{\Gamma}{2\pi} \frac{y}{x^2 + y^2}, \quad v = \frac{\Gamma}{2\pi} \frac{x}{x^2 + y^2}$$

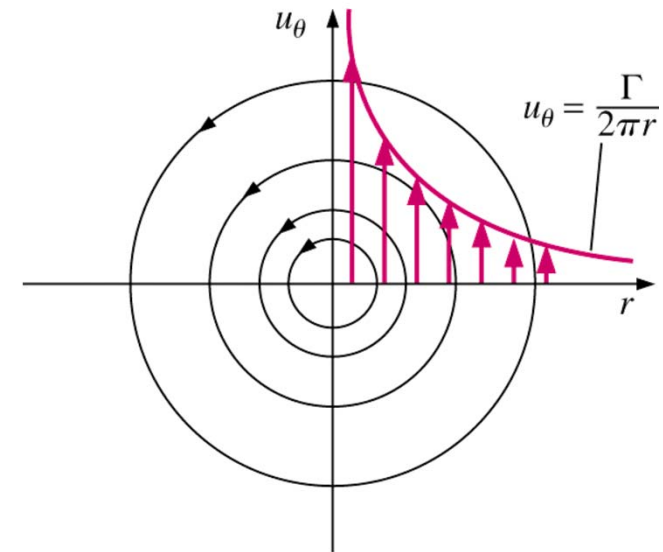
Is this flow rotational or irrotational? Will the fluid element deform or not?

**Solution:**

$$\omega_x = \omega_y = 0, \quad \omega_z = \frac{1}{2} \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) = 0$$

$$\varepsilon_{xx} = \frac{\Gamma}{2\pi} \frac{xy}{(x^2 + y^2)} = -\varepsilon_{yy} \neq 0, \quad \varepsilon_{zz} \neq 0$$

$$\varepsilon_{xy} = \varepsilon_{yx} = \varepsilon_{zx} = 0$$

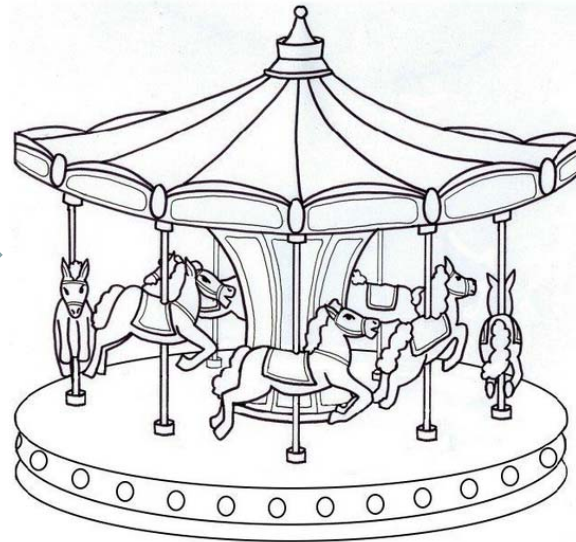
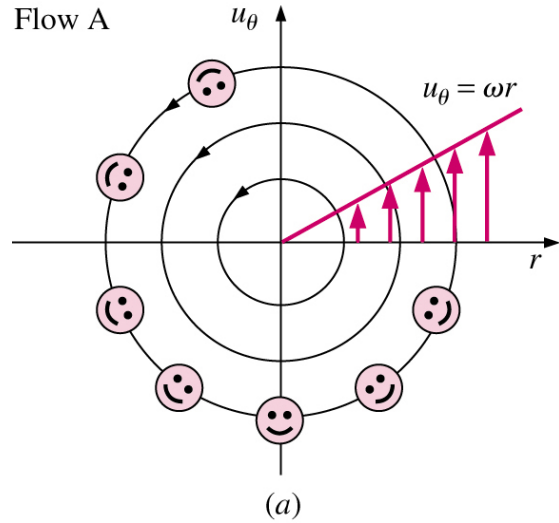


The flow is irrotational but deformed, can be used to describe the flow out of the core region of a tornado.

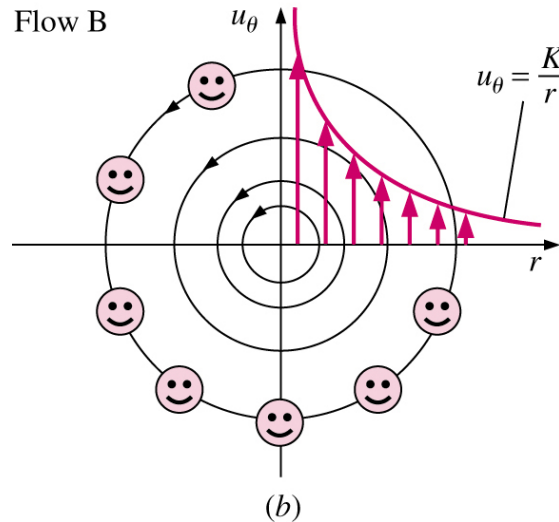


# 2.4 Rotational and Irrotational Flows

Not all flows with circular streamlines are rotational



rotational, no deformation; the flow is irrotational.



irrotational, deformation; the flow is rotational.



# 2.4 Rotational and Irrotational Flows

## Application 4

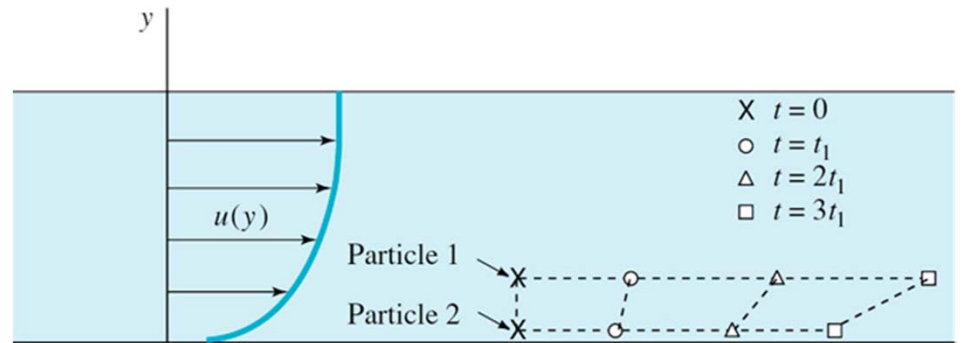
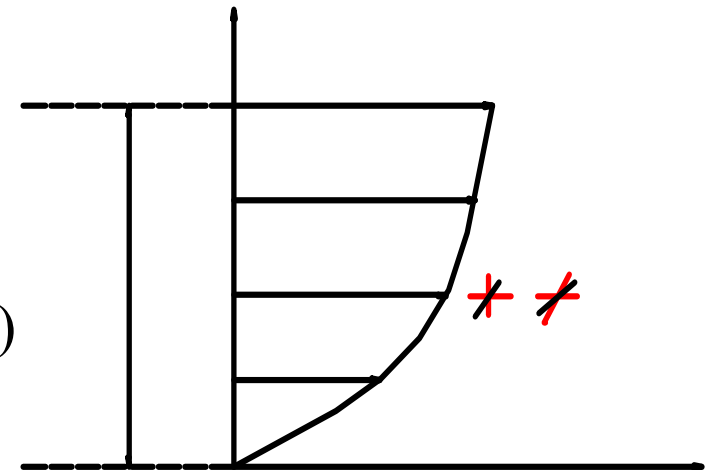
Consider a linear flow:  $u = \frac{v_{\max}}{h} (2y - y^2/h), \quad v = 0$

**Solution:**

$$\epsilon_{xx} = \epsilon_{yy} = \epsilon_{zz} = 0$$

$$\omega_x = \omega_y = 0, \quad \omega_z = \frac{1}{2} \left( \frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y} \right) = \frac{v_{\max}}{h} (1 - y/h)$$

$$\epsilon_{xy} = \frac{1}{2} \left( \frac{\partial v_y}{\partial x} + \frac{\partial v_x}{\partial y} \right) = \frac{v_{\max}}{h} \left( 1 - \frac{y}{h} \right) \neq 0$$



This is a rotational flow with deformation.





## 2.4 Rotational and Irrotational Flows

### Application 5

Consider a uniform linear motion of a fluid element:

$$u = v_0 = \text{const}, \quad v = 0$$

**Solution:**

$$\varepsilon_{xx} = \varepsilon_{yy} = \varepsilon_{zz} = 0$$

$$\varepsilon_{xy} = \varepsilon_{yz} = \varepsilon_{zx} = 0$$

$$\omega_x = \omega_y = \omega_z = 0$$

This is a irrotational flow without any deformation.

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## 2.5 Velocity Potential

- ◆ *Velocity potential*  
—— **for irrotational flow**
  
  - ◆ *Stream function*  
—— **for incompressible flow**
-



# 2.5 Velocity Potential

According to Green's theorem: let  $P, Q, R$  be functions of  $(x, y, z)$  and have **continuous** first-order partial derivatives

$$\frac{\partial P}{\partial y}, \frac{\partial P}{\partial z}, \frac{\partial Q}{\partial z}, \frac{\partial Q}{\partial x}, \frac{\partial R}{\partial x}, \frac{\partial R}{\partial y}, \dots$$

in a simple **closed curve** and its bounded **region**. If the following equations satisfied in the region:

$$\left. \begin{aligned} \frac{\partial Q}{\partial z} &= \frac{\partial R}{\partial y} \\ \frac{\partial R}{\partial x} &= \frac{\partial P}{\partial z} \\ \frac{\partial P}{\partial y} &= \frac{\partial Q}{\partial x} \end{aligned} \right\}$$



Then there must be a function defined by the **line integral** below. This function is **potential**, and is called **potential function**:

$$F(x, y, z)$$



$$F(x, y, z) = \int Pdx + Qdy + Rdz$$



## 2.5 Velocity Potential

The integral is **not** path-dependent, and has following relationships:

$$\left. \begin{aligned} \frac{\partial F}{\partial x} &= P \\ \frac{\partial F}{\partial y} &= Q \\ \frac{\partial F}{\partial z} &= R \end{aligned} \right\}$$

$$F(x, y, z) = \int \frac{\partial F}{\partial x} dx + \frac{\partial F}{\partial y} dy + \frac{\partial F}{\partial z} dz$$

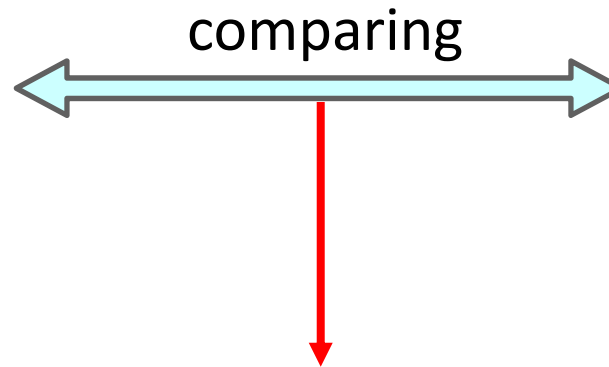
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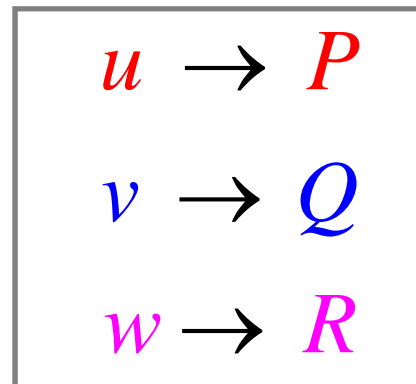
# 2.5 Velocity Potential

For an *irrotational flow*,  $\omega=0$ , thus:

$$\left. \begin{aligned} \frac{\partial v}{\partial z} &= \frac{\partial w}{\partial y} \\ \frac{\partial w}{\partial x} &= \frac{\partial u}{\partial z} \\ \frac{\partial u}{\partial y} &= \frac{\partial v}{\partial x} \end{aligned} \right\}$$



$$\left. \begin{aligned} \frac{\partial Q}{\partial z} &= \frac{\partial R}{\partial y} \\ \frac{\partial R}{\partial x} &= \frac{\partial P}{\partial z} \\ \frac{\partial P}{\partial y} &= \frac{\partial Q}{\partial x} \end{aligned} \right\}$$





## 2.5 Velocity Potential

Thus, there is a function:

$$\phi(x, y, z; t) = \int u dx + v dy + w dz$$

With the relationships:

$$\left. \begin{aligned} \frac{\partial \phi}{\partial x} &= u \\ \frac{\partial \phi}{\partial y} &= v \\ \frac{\partial \phi}{\partial z} &= w \end{aligned} \right\} \text{ i.e., } \mathbf{V} = \nabla \phi$$

$\phi$  is called the **velocity potential**. A flow has the velocity potential is called **potential flow**.

$$\text{Irrotational} \Leftrightarrow \nabla \times \mathbf{V} = \mathbf{0} \Leftrightarrow \phi \Leftrightarrow \text{Potential flow}$$



# 2.5 Velocity Potential

## Significance of velocity potential:

Velocity potential  $\phi$  is a **scalar** quantity with one component only:

$$\phi(x, y, z; t) = \int u dx + v dy + w dz$$

Velocity  $\mathbf{V}$  is a **vector** quantity with three components:

$$\left. \begin{aligned} \frac{\partial \phi}{\partial x} &= u \\ \frac{\partial \phi}{\partial y} &= v \\ \frac{\partial \phi}{\partial z} &= w \end{aligned} \right\}$$

Irrotational velocity field  $\Leftrightarrow$  Potential flow



## 2.5 Velocity Potential

### Application

The velocity field of a rotational flow is given by:

$$u = 2(x-a)y, \quad v = (x+a)^2 - y^2$$

where  $a$  is a constant. Consider an irrotational flow, its linear strain rate and shear strain rate are identical to those in rotational flow. The velocity at the origin is 0, i.e., when  $x = y = 0$ ,  $u = v = 0$ . Determine the velocity expression and the velocity potential of this irrotational flow.

**Solution:** for the given rotational flow

$$\text{linear strain rate: } \varepsilon_{xx} = \frac{\partial u}{\partial x} = 2y, \quad \varepsilon_{yy} = \frac{\partial v}{\partial y} = -2y \quad (\text{a})$$

$$\text{shear strain rate: } \varepsilon_{xy} = \frac{1}{2} \left( \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) = 2x \Rightarrow \frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} = 4x \quad (\text{b})$$

The linear strain rate and shear strain rate of the irrotational flow are the same, and the irrotational flow has to satisfy:

$$\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} = 0 \quad (\text{c})$$





# 2.5 Velocity Potential

From (c)+(b) :  $\frac{\partial v}{\partial x} = 2x$  i.e.,  $v = x^2 + f(y)$

Substituting it into (a):  $f'(y) = -2y$ , i.e.,  $f(y) = -y^2 + C_1$

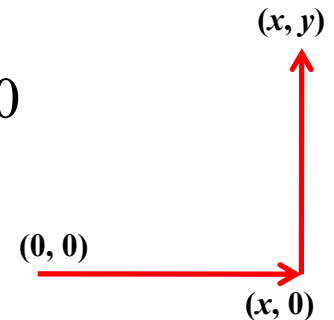
From (c)-(b):  $\frac{\partial u}{\partial y} = 2x$  i.e.,  $u = 2xy + g(x)$

Substituting it into (a):  $g'(x) = 0$ , i.e.,  $g(x) = C_2$

$C_1$  and  $C_2$  are integral constants. When  $x = y = 0$ ,  $u = v = 0$

$$\Rightarrow C_1 = C_2 = 0$$

Thus, the velocity is:  $u = 2xy$ ,  $v = x^2 - y^2$



The velocity potential is:

$$\begin{aligned} \phi &= \int u \, dx + v \, dy = \int 2xy \, dx + (x^2 - y^2) \, dy \\ &= \int_{(0,0)}^{(x,0)} + \int_{(x,0)}^{(x,y)} = 0 + \int_{(x,0)}^{(x,y)} (x^2 - y^2) \, dy = x^2 y - \frac{1}{3} y^3 \end{aligned}$$



# Review: Key Points in Chapter 2

- **Two ways of describing a fluid flow:**

**Lagrangian description, Eulerian description**

- **Material derivative:**  $\frac{D(\quad)}{Dt} = \frac{\partial(\quad)}{\partial t} + (\mathbf{v} \cdot \nabla)(\quad)$

$$\begin{aligned} \vec{a}_{\text{particle}} &= \frac{d\vec{V}_{\text{particle}}}{dt} = \frac{d\vec{V}}{dt} = \frac{d\vec{V}(x_{\text{particle}}, y_{\text{particle}}, z_{\text{particle}}, t)}{dt} \\ &= \frac{\partial \vec{V}}{\partial t} \frac{dt}{dt} + \frac{\partial \vec{V}}{\partial x_{\text{particle}}} \frac{dx_{\text{particle}}}{dt} + \frac{\partial \vec{V}}{\partial y_{\text{particle}}} \frac{dy_{\text{particle}}}{dt} + \frac{\partial \vec{V}}{\partial z_{\text{particle}}} \frac{dz_{\text{particle}}}{dt} \end{aligned}$$

$$\Rightarrow \underbrace{\vec{a}_{\text{particle}}(x, y, z, t)}_{\text{Lagrangian}} = \frac{d\vec{V}}{dt} = \underbrace{\frac{\partial \vec{V}}{\partial t} + u \frac{\partial \vec{V}}{\partial x} + v \frac{\partial \vec{V}}{\partial y} + w \frac{\partial \vec{V}}{\partial z}}_{\text{Eulerian}}$$



# Review: Key Points in Chapter 2

- **Pathline equation:**  $\frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w} = dt$
- **Streamline equation:**  $\frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w}$

Pathlines and streamlines are identical in **steady flows**

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# Review: Key Points in Chapter 2

- **Motion or deformation of fluid elements**

$$\boldsymbol{\omega} = \frac{1}{2} \nabla \times \mathbf{V} = \omega_x \vec{i} + \omega_y \vec{j} + \omega_z \vec{k} = \left( \frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) \vec{i} + \left( \frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) \vec{j} + \left( \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) \vec{k}$$

- **Helmholtz decomposition**

$$\mathbf{V} = \mathbf{V}_0 + \mathbf{E} \cdot \delta \mathbf{r} + \boldsymbol{\omega} \times \delta \mathbf{r} \quad \mathbf{E} = \varepsilon_{ij} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

- **Rotational and irrotational flows**

$$\boldsymbol{\Omega} = (\Omega_x, \Omega_y, \Omega_z) = 0$$

- **Velocity potential: irrotational flows**

$$\mathbf{V} = \nabla \phi, \quad \phi(x, y, z; t) = \int u dx + v dy + w dz \text{ —————}$$



# Chapter 3

# Fluid Dynamics

*Fluid dynamics*: study of the motion of fluids considering the forces and moments that cause the motion.

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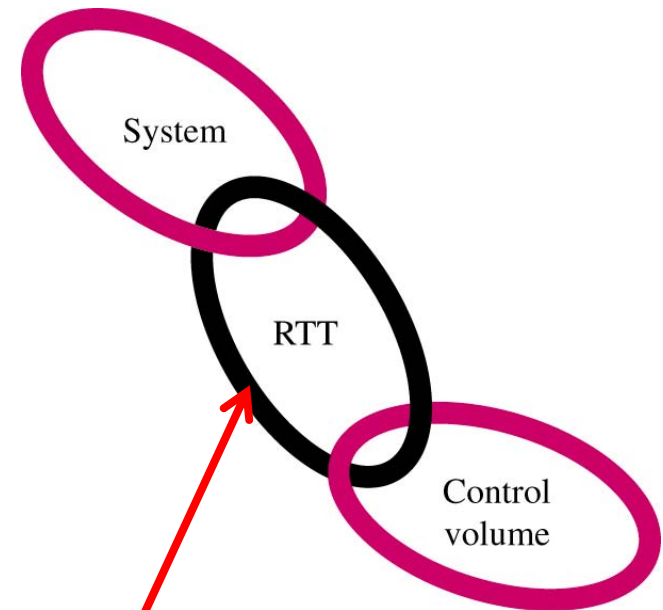


# 3.1 Representation of Fluid Flow

Two approaches in fluid dynamics: **system approach** and **control volume approach**

(1) **System** (material volume) approach: follows the fluid as it moves and deforms; no mass crosses the boundary (**Lagrangian description**)

(2) **Control volume** approach: considers the changes in a certain fixed volume; mass can cross the boundary (**Eulerian description**)



**Reynolds Transport Theorem (RTT)**

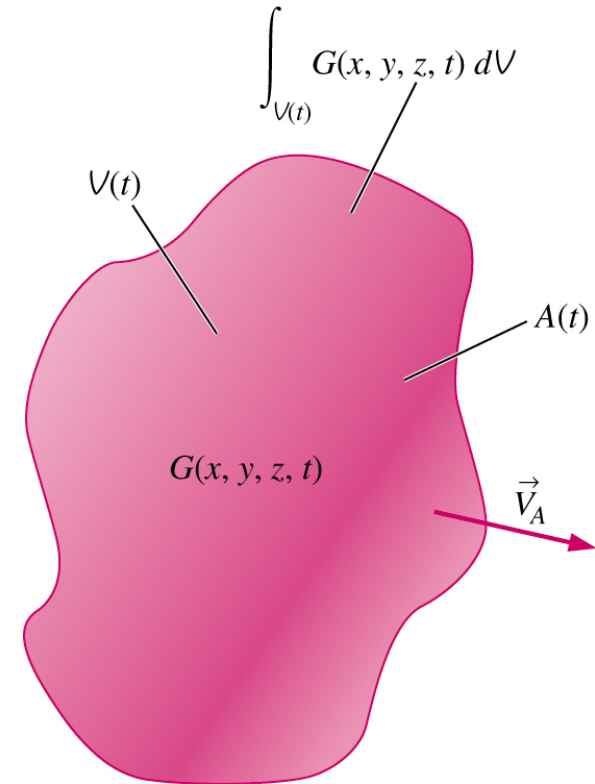


# 3.1 Representation of Fluid Flow

**System:** a collection of matter of fixed identity (always the same fluid particles), which may move, flow, and interact with its surroundings.

**Material volume:** a volume that contains the same fluid as it moves and deforms following the motion of the fluid.

**Material surface:** an enclosing surface of a material volume; no fluid particles can cross it.



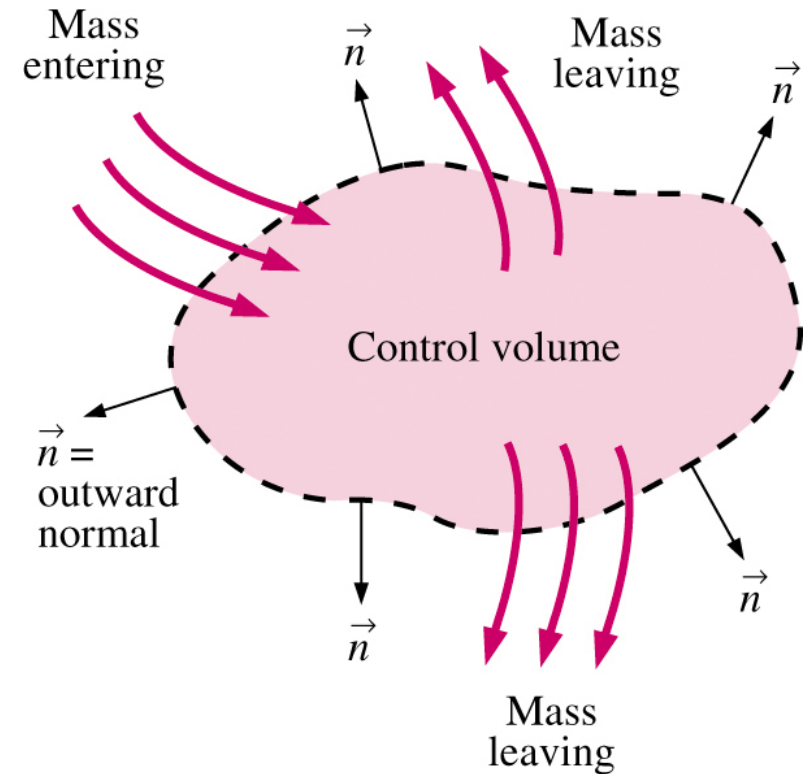


## 3.2 Reynolds Transport Theorem

**Control volume:** a volume in space (a geometric entity, independent of mass) through which fluid may flow.

**Control volume:** a volume of fluid in a flow field, usually **fixed** in space, to be **occupied** by different fluid particles at different times.

**Control surface:** imaginary or physical enclosing surface of a control volume, fluid particles **can cross it**.

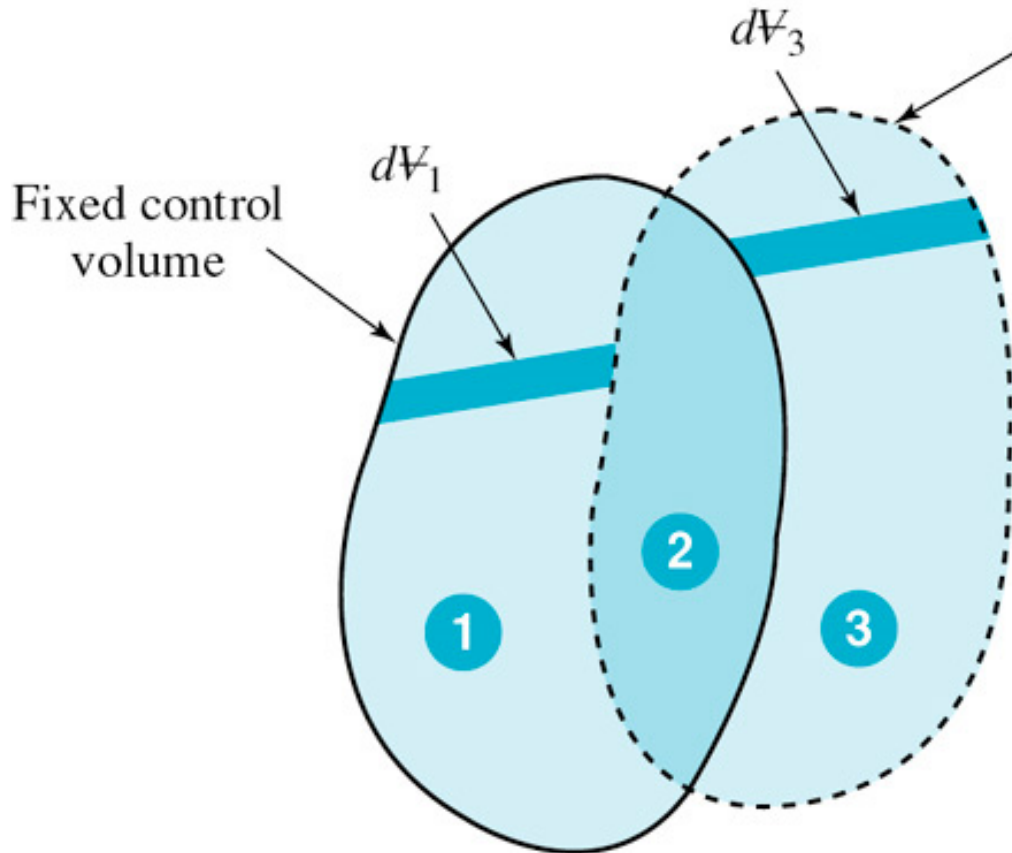


$$\dot{B}_{\text{net}} = \dot{B}_{\text{out}} - \dot{B}_{\text{in}} = \int_{\text{CS}} \rho b \vec{V} \cdot \vec{n} dA$$





# 3.2 Reynolds Transport Theorem



System

Fixed control volume

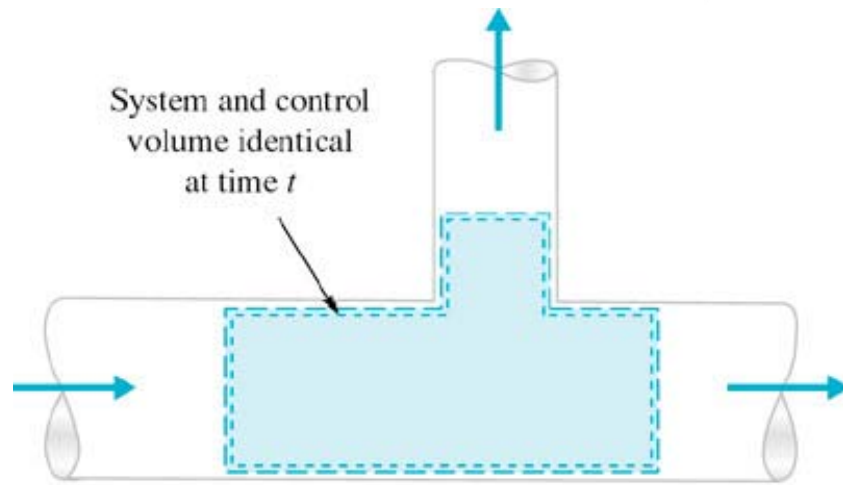
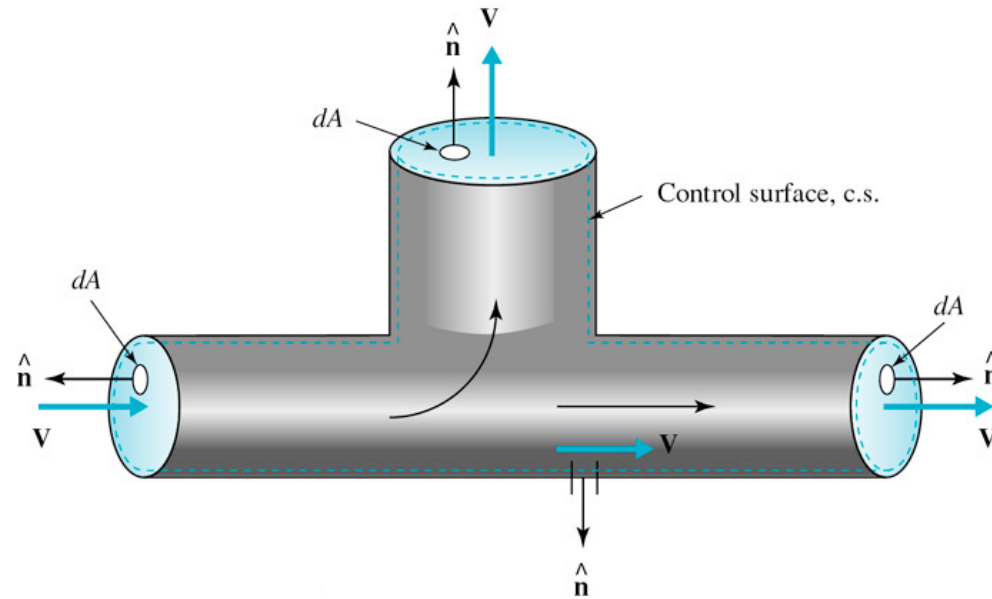
Fixed control volume occupies 1 and 2.

System at time  $t$  occupies volumes 1 and 2.

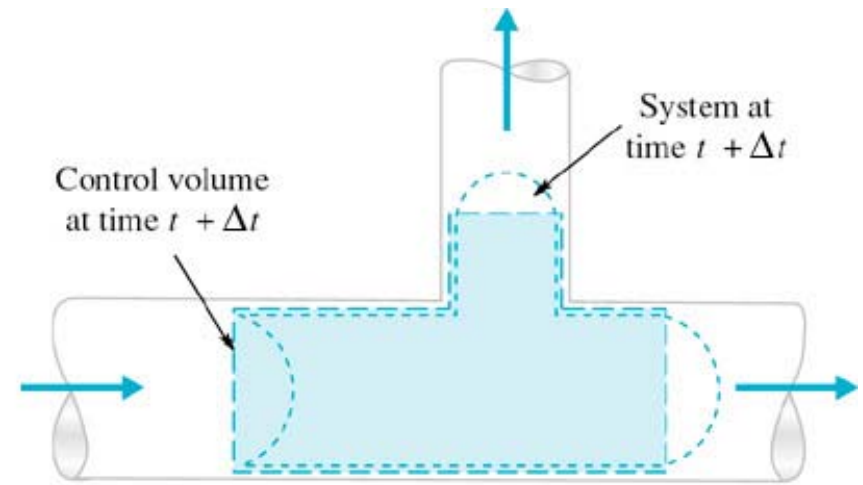
System at time  $t + \Delta t$  occupies volumes 2 and 3.



# 3.2 Reynolds Transport Theorem



(a)



(b)



# 3.2 Reynolds Transport Theorem

## Reynolds Transport Theorem

Any quantity  $G$  satisfies the relationship between **material volume** and **control volume**:

$$\frac{d}{dt} \iiint_{MV} G dV = \frac{\partial}{\partial t} \iiint_{CV} G dV + \iint_{CS} G \mathbf{V} \cdot \mathbf{n} dA$$

rate of change of the property  $G$  within the material volume

local rate of change of the property within the fixed control volume that happens to coincide with the material volume at that instant

net out-flux of the property across the entire control surface

$\rho$  = density of fluid

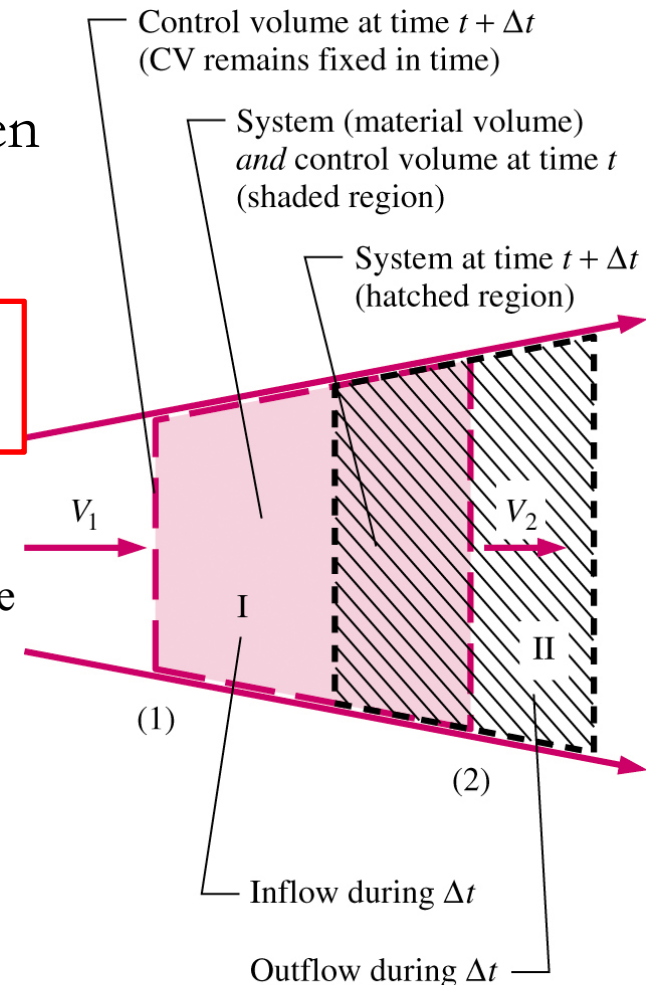
$G$  = an intensive property of fluid

$MV$  = material volume that happens to coincide with  $CV$  at time  $t$

$CV$  = control volume (fixed in space)

$CS$  = control surface

$\mathbf{n}$  = unit outward normal to  $CS$



At time  $t$ : Sys = CV  
At time  $t + \Delta t$ : Sys = CV - I + II



# 3.2 Reynolds Transport Theorem

For a material volume, after a time period  $dt$ :

$$\left[ \iiint_{MV} G(\mathbf{x}, t) dV \right]_{t+dt} = \iiint_{MV(t+dt)} G(\mathbf{x}, t+dt) dV = \iiint_{MV(t+dt)} \left[ G(\mathbf{x}, t) + \frac{\partial G}{\partial t} dt + \cancel{O(dt)^2} \right] dV$$

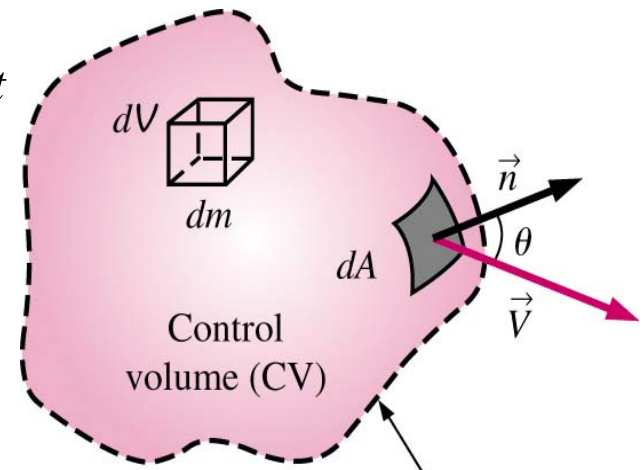
The change of material volume in  $dt$  is:

$$\iiint_{MV(t+dt)} ( ) = \iiint_{MV} ( ) + \iiint_{\Delta V} ( ) = \iiint_{CV} ( ) + \iint_{CS} ( ) \mathbf{V} \cdot \mathbf{n} dS dt$$

Thus:

$$\begin{aligned} \left[ \iiint_{MV} G(\mathbf{x}, t) dV \right]_{t+dt} &= \iiint_{MV(t+dt)} \left[ G(\mathbf{x}, t) + \frac{\partial G}{\partial t} dt \right] dV \\ &= \iiint_{CV} \left[ G(\mathbf{x}, t) + \frac{\partial G}{\partial t} dt \right] dV + \iint_{CS} \left[ G(\mathbf{x}, t) + \frac{\partial G}{\partial t} dt \right] \mathbf{V} \cdot \mathbf{n} dS dt \\ &= \iiint_{CV} G(\mathbf{x}, t) dV + \left[ \iiint_{CV} \frac{\partial G}{\partial t} dV + \iint_{CS} G(\mathbf{x}, t) \mathbf{V} \cdot \mathbf{n} dS \right] dt \end{aligned}$$

omit 2<sup>nd</sup> order quantities



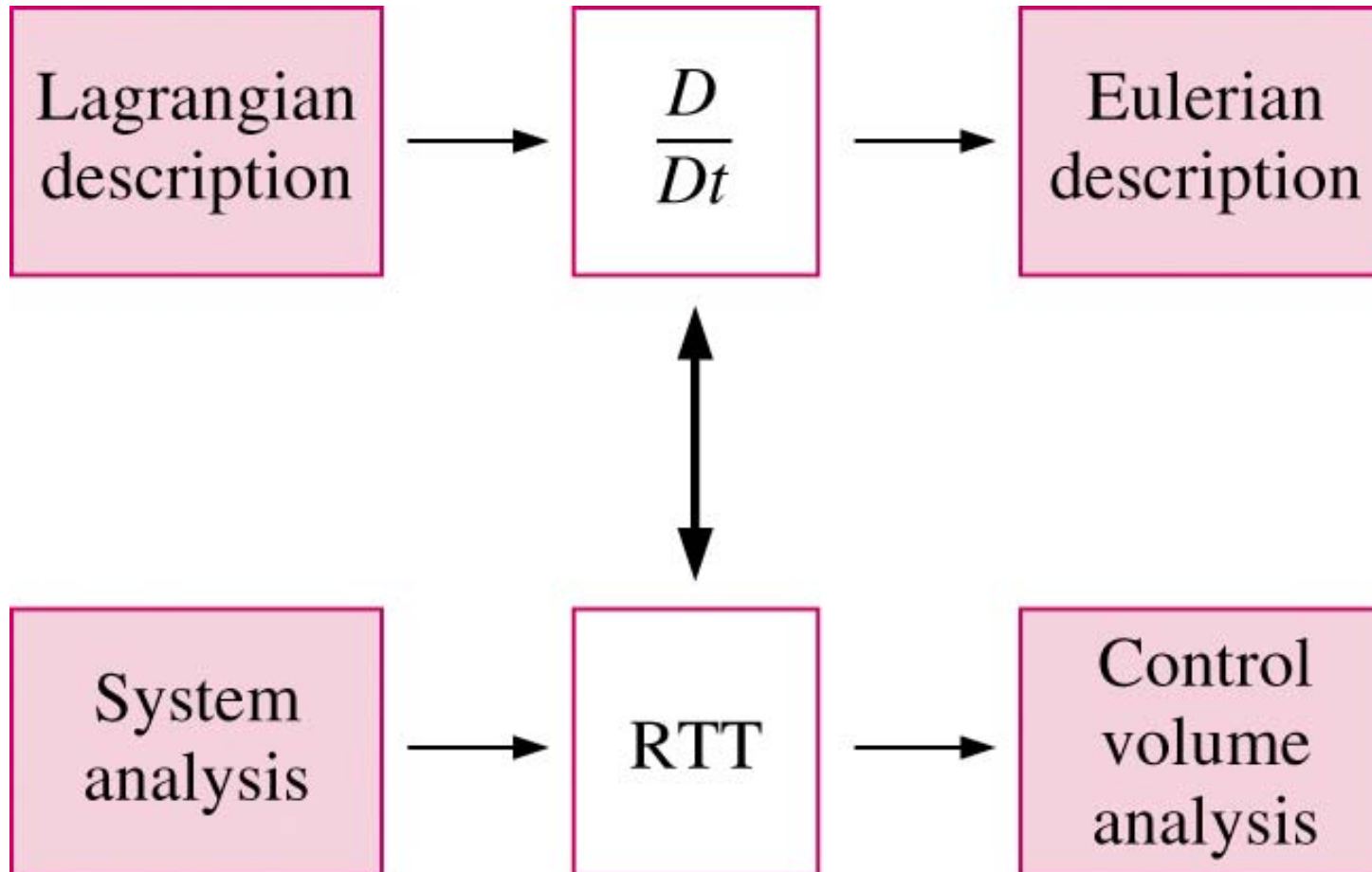
RTT can be derived from the equation above:

$$\frac{d}{dt} \iiint_{MV} G dV = \left\{ \left[ \iiint_{MV} G dV \right]_{t+dt} - \iiint_{MV} G dV \right\} / dt = \iiint_{CV} \frac{\partial G}{\partial t} dV + \iint_{CS} G \mathbf{V} \cdot \mathbf{n} dS$$

Control surface (CS)



## 3.2 Reynolds Transport Theorem





## 3.3 Continuity Equation

**Continuity Equation:** conservation of mass (mass of a system is neither be created nor destroyed)

In RTT equation, if the quantity is mass, i.e.,  $G = \rho$ , then:

$$\text{L.H.S.} \quad \frac{d}{dt} \iiint_{MV} \rho dV = \frac{d}{dt} (\text{mass in } MV) = 0$$

(From the definition of MV: it always contains the same fluids)

$$\begin{aligned} \text{R.H.S.} \quad & \frac{\partial}{\partial t} \iiint_{CV} \rho dV + \iint_{CS} \rho \mathbf{V} \cdot \mathbf{n} dA \\ &= \underbrace{\iiint_{CV} \frac{\partial \rho}{\partial t} dV}_{CV \text{ is stationary}} + \underbrace{\iiint_{CV} \nabla \cdot (\rho \mathbf{V}) dV}_{\text{by Gauss theorem}} \end{aligned}$$