



CMHL SJTU COMPUTATIONAL MARINE HYDRODYNAMICS LAB 上海交大船舶与海洋工程计算水动力学研究中心

Class-9

NA26018

Finite Element Analysis of Solids and Fluids



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The finite element (FE) numerical computation of incompressible Navier–Stokes equations (NS) suffers from two main sources of numerical instabilities arising from the associated Galerkin problem:

- Equal order finite elements approximation for pressure and velocity, do not satisfy the Babuška–Brezzi condition and leads to instability on the discrete pressure (also called spurious pressure)
- 2. The advection term in the Navier–Stokes equations can produce oscillations in the velocity field (also called spurious velocity)

Such spurious velocity oscillations become more evident for advectiondominated (i.e., high Reynolds number) flows

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The streamline upwind Petrov–Galerkin pressure-stabilizing Petrov–Galerkin (SUPG/PSPG) formulation for incompressible Navier–Stokes equations can be used for

- finite element computations of high Reynolds number incompressible flow,
- using equal order of finite element space (for velocity and pressure) by <u>introducing additional stabilization terms</u> in the Navier–Stokes Galerkin formulation

Consider the governing equation of incompressible viscous flows:

$$\rho \left(\frac{\partial \mathbf{u}}{\partial t} + \mathbf{u} \cdot \nabla \mathbf{u} - \mathbf{f} \right) - \nabla \cdot \mathbf{\sigma} = 0$$
$$\nabla \cdot \mathbf{u} = 0$$

$$\boldsymbol{\sigma} = \boldsymbol{\tau} - p \boldsymbol{I}$$

For Newtonian fluid,

$$\mathbf{\tau} = 2 \,\mu \mathbf{D} \qquad \mathbf{D} = \frac{1}{2} (\nabla \mathbf{u} + (\nabla \mathbf{u})^{\mathrm{T}})$$

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The variational formulations with the SUPG and PSPG stabilization terms will be described

 Note: These formulations are based on finite element discretization in space only, rather than in both space and time

$$S_{u}^{h} = \left\{ u^{h} \mid u^{h} \in \left(\mathbf{H}^{1h} \right)^{d}, u^{h} = \hat{u}^{h} \text{ on } \Gamma_{u} \right\}$$
$$V_{u}^{h} = \left\{ w^{h} \mid u^{h} \in \left(\mathbf{H}^{1h} \right)^{d}, w^{h} = 0 \text{ on } \Gamma_{u} \right\}$$
$$S_{p}^{h} = V_{p}^{h} = \left\{ q^{h} \mid q^{h} \in \left(\mathbf{H}^{1h} \right) \right\}$$

Rewrite the momentum equation into tensor format

$$\rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = \frac{\partial \sigma_{ij}}{\partial x_j} + \rho f_i$$



Multiply the velocity test function w_i into tensor format, we obtain

$$\int_{\Omega} w_i \rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) d\Omega = \int_{\Omega} w_i \frac{\partial \sigma_{ij}}{\partial x_j} d\Omega + \int_{\Omega} \rho w_i f_i d\Omega$$

The first term of the Rhs for above Eq., can be expanded as

$$\int_{\Omega} w_i \frac{\partial \sigma_{ij}}{\partial x_j} d\Omega = \int_{\Omega} \left[\frac{\partial}{\partial x_j} (w_i \sigma_{ij}) - \sigma_{ij} \frac{\partial w_i}{\partial x_j} \right] d\Omega$$
$$= \oint_{\Gamma_u \cup \Gamma_h \cup \Gamma_d} w_i \sigma_{ij} n_j d\Gamma - \int_{\Omega} \sigma_{ij} \frac{\partial w_i}{\partial x_j} d\Omega$$

$$=\oint_{\Gamma_h} w_i \hat{h}_i d\Gamma + \oint_{\Gamma_d^+} w_i (\sigma_{ij} n_j)^+ d\Gamma + \oint_{\Gamma_d^-} w_i (\sigma_{ij} n_j)^- d\Gamma - \int_{\Omega} \sigma_{ij} \frac{\partial w_i}{\partial x_j} d\Omega$$

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$$= \oint_{\Gamma_{h}} w_{i} \hat{h}_{i} d\Gamma + \oint_{\Gamma_{d}^{+}} w_{i} (\sigma_{ij} n_{j})^{+} d\Gamma + \oint_{\Gamma_{d}^{-}} w_{i} (\sigma_{ij} n_{j})^{-} d\Gamma - \int_{\Omega} \sigma_{ij} \frac{\partial w_{i}}{\partial x_{j}} d\Omega$$

$$= \oint_{\Gamma_{h}} w_{i} \hat{h}_{i} d\Gamma + \oint_{\Gamma_{d}} w_{i} \hat{n}_{j} (\sigma_{ij}^{+} + \sigma_{ij}^{-}) d\Gamma - \int_{\Omega} \sigma_{ij} \frac{\partial w_{i}}{\partial x_{j}} d\Omega$$

$$= \oint_{\Gamma_{h}} w_{i} \hat{h}_{i} d\Gamma + \oint_{\Gamma_{d}} \gamma \kappa w_{i} \hat{n}_{j} d\Gamma - \int_{\Omega} \sigma_{ij} \frac{\partial w_{i}}{\partial x_{j}} d\Omega$$
(a)

Note: if surface tension is considered(for multiphase flow). Otherwise, this term is zero

Multiply the pressure test function \mathbf{p}_i into tensor format, we obtain

$$\int_{\Omega} q_i \left(\frac{\partial u_j}{\partial x_j}\right) d\Omega = 0$$
 (b)

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Combing (a) and (b), we obtain:

$$\int_{\Omega} w_i \rho \left(\frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) d\Omega + \int_{\Omega} \sigma_{ij} \frac{\partial w_i}{\partial x_j} d\Omega - \oint_{\Gamma_h} w_i \hat{h}_i d\Gamma + \int_{\Omega} q_i \left(\frac{\partial u_j}{\partial x_j} \right) d\Omega = \int_{\Omega} \rho w_i f_i \ d\Omega + \oint_{\Gamma_d} \gamma \kappa w_i \hat{n}_j d\Gamma$$

Written into vector form, we obtain:

$$\int_{\Omega} \mathbf{w}^{h} \rho \left(\frac{\partial \mathbf{u}^{h}}{\partial t} + \mathbf{u}^{h} \cdot \nabla \mathbf{u}^{h} \right) d\Omega + \int_{\Omega} \varepsilon(\mathbf{w}^{h}) : \sigma(\mathbf{u}^{h}, p^{h}) d\Omega$$
$$- \oint_{\Gamma_{h}} \mathbf{w}^{h} \hat{h} d\Gamma + \int_{\Omega} q^{h} \nabla \cdot \mathbf{u}^{h} d\Omega = \int_{\Omega} \rho \mathbf{w}^{h} \cdot \mathbf{f} \ d\Omega + \oint_{\Gamma_{d}} \gamma \kappa \mathbf{w}^{h} \cdot \hat{\mathbf{n}}_{j} d\Gamma$$

COMPUTATIONAL MARINE HYDRODYNAMICS LAB SHANGHAI JIAO TONG UNIVERSITY Use the SUPG/PSPG by Tezduyar and Osawa, above Eq. can be given by

$$\int_{\Omega} \mathbf{w}^{h} \cdot \rho \left(\frac{\partial \mathbf{u}^{h}}{\partial t} + \mathbf{u}^{h} \cdot \nabla \mathbf{u}^{h} - \mathbf{f} \right) d\Omega + \int_{\Omega} \boldsymbol{\varepsilon}(\mathbf{w}^{h}) : \boldsymbol{\sigma}(\mathbf{p}^{h}, \mathbf{u}^{h}) d\Omega - \int_{\Gamma} \mathbf{w}^{h} \cdot \hat{\mathbf{h}} d\Gamma + \int_{\Omega} \mathbf{q}^{h} \nabla \cdot \mathbf{u}^{h} d\Omega$$

$$+ \sum_{e=1}^{n_{e1}} \int_{\Omega^{e}} \frac{1}{\rho} \left[\tau_{SUPG} \rho \, \mathbf{u}^{h} \cdot \nabla \mathbf{w}^{h} + \tau_{PSPG} \nabla \mathbf{q}^{h} \right] \cdot \left[\rho \left(\frac{\partial \mathbf{u}^{h}}{\partial t} + \mathbf{u}^{h} \cdot \nabla \mathbf{u}^{h} \right) - \nabla \cdot \boldsymbol{\sigma}(\mathbf{p}^{h}, \mathbf{u}^{h}) - \rho \, \mathbf{f} \right] d\Omega^{e} = 0$$

$$(\mathbf{c})$$

 w^h and q^h are test function for velocity and pressure.

The preceding 4 terms are from weak form of Galerkin method, others are from stabilizing form introduced by the SUPG/PSPG

 τ_{SUPG} τ_{PSPG} are parameters for stablizing

$$\tau_{SUPG} = \tau_{PSPG} = \left[\left(\frac{2 \parallel \mathbf{u}^h \parallel}{h} \right)^2 + 9 \left(\frac{4\mu}{h^2} \right)^2 \right]^{-\frac{1}{2}}$$

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Interpolation for velocity and pressure can be given by

$$\mathbf{u}^{h} = \overline{\mathbf{N}}\mathbf{v} \qquad p^{h} = \mathbf{N}p$$
$$\mathbf{N} = [N_{1}, N_{2}, \dots, N_{n}]$$

Eq. (c) leads to the following non-linear ordinary differential equations

$$(\mathbf{M} + \mathbf{M}_{\delta})\mathbf{a} + \mathbf{C}(\mathbf{v}) + \mathbf{C}_{\delta}(\mathbf{v}) + (\mathbf{K} + \mathbf{K}_{\delta})\mathbf{v} - (\mathbf{G} + \mathbf{G}_{\delta})\mathbf{p} = (\mathbf{F} + \mathbf{F}_{\delta})$$

$$\mathbf{G}^{T}\mathbf{v} + \mathbf{M}_{\epsilon}\mathbf{a} + \mathbf{C}_{\epsilon}(\mathbf{v}) + \mathbf{K}_{\epsilon}\mathbf{v} + \mathbf{G}_{\epsilon}\mathbf{p} = \mathbf{E} + \mathbf{E}_{\epsilon}$$

$$\mathbf{M} = \int_{\Omega} \rho \overline{\mathbf{N}}^{T} \overline{\mathbf{N}} dV$$

$$\mathbf{M}_{\delta} = \int_{\Omega} \tau_{SUPG} \rho \mathbf{u} \nabla \overline{\mathbf{N}}^{T} \overline{\mathbf{N}} dV$$

$$\mathbf{M}_{\epsilon} = \int_{\Omega} \tau_{PSPG} \nabla \overline{\mathbf{N}}^{T} \overline{\mathbf{N}} dV$$

Acceleration term

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SUPG/PSPG Method for Incompressible Flow

$$\mathbf{N}(\mathbf{u}) = \int_{\Omega} \rho \overline{\mathbf{N}}^{\mathrm{T}} \mathbf{u} \cdot \nabla \overline{\mathbf{N}} dV \mathbf{u}$$

$$\mathbf{N}_{\delta}(\mathbf{u}) = \int_{\Omega} \tau_{SUPG} \rho \mathbf{u} \nabla \overline{\mathbf{N}}^{\mathrm{T}} \mathbf{u} \cdot \nabla \overline{\mathbf{N}} dV \mathbf{u}$$

$$\mathbf{N}_{\varepsilon}(\mathbf{u}) = \int \tau_{PSPG} \nabla \overline{\mathbf{N}}^{\mathrm{T}} \mathbf{u} \cdot \nabla \overline{\mathbf{N}} dV \mathbf{u}$$

$$\mathbf{K} = \int_{\Omega} \mathbf{B}^{\mathrm{T}} \mu (\mathbf{I}_{0} - \frac{2}{3} \mathrm{mm}^{\mathrm{T}}) \mathbf{B} dV \mathbf{u}$$

$$\mathbf{K}_{\delta} = \int_{\Omega} \tau_{SUPG} \nabla \overline{\mathbf{N}}^{\mathrm{T}} \mathbf{u} \mathbf{B}^{\mathrm{T}} \mu (\mathbf{I}_{0} - \frac{2}{3} \mathrm{mm}^{\mathrm{T}}) \mathbf{B} dV \mathbf{u}$$

$$\mathbf{G}_{\delta} = \int_{\Omega} (\nabla \overline{\mathbf{N}})^{\mathrm{T}} \overline{\mathbf{N}} dV \mathbf{u}$$

$$\mathbf{G}_{\varepsilon} = \int_{\Omega} \tau_{SUPG} \rho \mathbf{u} (\nabla \overline{\mathbf{N}})^{\mathrm{T}} \nabla \overline{\mathbf{N}} dV \mathbf{u}$$

$$\mathbf{Pressure term}$$

$$\mathbf{F} = \int_{\Omega} \overline{\mathbf{N}}^{\mathrm{T}} \rho \mathbf{g} dV + \int_{\Gamma} \overline{\mathbf{N}}^{\mathrm{T}} \mathbf{t}_{s} dS \quad \mathbf{E} = \int_{\Omega} (\nabla \overline{\mathbf{N}})^{\mathrm{T}} \mathbf{g} dV \quad \mathbf{Force and boundary term}$$
$$\mathbf{F}_{\delta} = \int_{\Omega} \tau_{SUPG} \mathbf{u} \nabla \overline{\mathbf{N}}^{\mathrm{T}} \rho \mathbf{g} dV \quad \mathbf{E}_{\varepsilon} = \int_{\Omega} \tau_{PSPG} (\nabla \overline{\mathbf{N}})^{\mathrm{T}} \mathbf{g} dV \quad \mathbf{F}_{\varepsilon}$$

where

$$\mathbf{B} = [\mathbf{B}_{1} \quad \mathbf{B}_{2} \quad \dots \quad \mathbf{B}_{n}]^{T} \quad \mathbf{B}_{I} = \begin{bmatrix} \frac{\partial N_{I}}{\partial x} & 0\\ 0 & \frac{\partial N_{I}}{\partial y}\\ \frac{\partial N_{I}}{\partial x} & \frac{\partial N_{I}}{\partial y} \end{bmatrix} \qquad \mathbf{m} = \begin{bmatrix} 1\\ 1\\ 0 \end{bmatrix} \qquad I_{0} = \begin{bmatrix} 2 & 0\\ 2 & 0\\ 0 & 1 \end{bmatrix}$$

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Solving procedure

Suppose the acceleration, velocity and pressure at $t + \Delta t$ have the following relations

$$\mathbf{a}^{t+\Delta t} = \mathbf{a}^t + \Delta \mathbf{a}, \qquad \frac{\mathbf{v}^{t+\Delta t} - \mathbf{v}^t}{\Delta t} = \alpha \cdot \mathbf{a}^{t+\Delta t} + (1-\alpha) \cdot \mathbf{a}^t, \qquad \mathbf{p}^{t+\Delta t} = \mathbf{p}^t + \Delta \mathbf{p}$$

Eq.(d) can be written in increment form

$$\mathbf{M}^* \Delta \mathbf{a} - \mathbf{G}^* \Delta \mathbf{p} = \mathbf{R}$$
$$(\mathbf{G}^T)^* \Delta \mathbf{a} - \mathbf{G}^*_{\varepsilon} \Delta \mathbf{p} = \mathbf{Q}$$

R, Q and other terms is given as



Solving procedure

 $\mathbf{R} = \mathbf{F} + \mathbf{F}_{\delta} - [(\mathbf{M} + \mathbf{M}_{\delta})\mathbf{a} + \mathbf{C}(\mathbf{v}) + \mathbf{C}_{\delta}(\mathbf{v}) + (\mathbf{K} + \mathbf{K}_{\delta})\mathbf{v} - (\mathbf{G} + \mathbf{G}_{\delta})\mathbf{p}]$ $\mathbf{Q} = \mathbf{E} + \mathbf{E}_{\varepsilon} - [\mathbf{G}^{T}\mathbf{v} + \mathbf{M}_{\varepsilon}\mathbf{a} + \mathbf{C}_{\varepsilon}(\mathbf{v}) + \mathbf{K}_{\varepsilon}\mathbf{v} - \mathbf{G}_{\varepsilon}\mathbf{p}]$

$$\mathbf{M}^{*} = \mathbf{M} + \mathbf{M}_{\delta} + \alpha \Delta t \left(\frac{\partial \mathbf{C}(\mathbf{v})}{\partial \mathbf{v}} + \frac{\partial \mathbf{C}_{\delta}(\mathbf{v})}{\partial \mathbf{v}} + \mathbf{K} + \mathbf{K}_{\delta} \right)$$
$$\mathbf{G}^{*} = \mathbf{G} + \mathbf{G}_{\delta}$$
$$(\mathbf{G}^{\mathsf{T}})^{*} = \mathbf{M}_{\varepsilon} + \alpha \Delta t \left(\frac{\partial \mathbf{C}(\mathbf{v})}{\partial \mathbf{v}} + \mathbf{K}_{\varepsilon} + \mathbf{G}^{\mathsf{T}} \right)$$

The increment Eqs. can be solved with initial guess

$$\mathbf{v}_{\mathbf{0}}^{t+\Delta t} = \mathbf{v}^{t} + \Delta t \mathbf{a}^{t}, \qquad \mathbf{a}_{\mathbf{0}}^{t+\Delta t} = \mathbf{a}^{t}, \qquad \mathbf{p}_{\mathbf{0}}^{t+\Delta t} = \mathbf{p}^{t}$$

Solutions can be updated iteratively by

$$\mathbf{a}_{i+1}^{t+\Delta t} = \mathbf{a}_{i}^{t+\Delta t} + \Delta \mathbf{a}, \qquad \mathbf{v}_{i+1}^{t+\Delta t} = \mathbf{v}_{i}^{t+\Delta t} + \Delta t \alpha \Delta \mathbf{a}, \qquad \mathbf{p}_{i+1}^{t+\Delta t} = \mathbf{p}_{i}^{t+\Delta t} + \Delta \mathbf{p}$$

For a in the incremental Eqs, if $a \ge 0.5$: unconditional stable



SUPG/PSPG Method for Incompressible Flow

Open source solvers by SUPG/PSPG: OOFEM



dam breaking problem - incompressible, free surface flow

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